

Topic: Thermal Neutron Cross-Section Measurements by Transmission Testing

Date: April 14, 2007

Purpose: To determine the total thermal neutron cross sections of various materials through thermal neutron transmission experiments

Location: UCD/ MNRC's Bay 4

Description of Neutron Beam:

Thermal neutron beam at UCD/ MNRC's Bay 4 is filtered by 11"-thick of sapphire crystal (Al_2O_3) with relatively low contamination of fast neutrons and gamma rays. This neutron beam is used for high quality neutron radiography of inspected parts and materials. The beam aperture is 1.25" x 1.25" and built with a 1"-thick B_4C piece. The exit beam size is 6" x 6" and it becomes about 9" x 9" at the fast shutter location. L/D ratio is 168 at the fast shutter and 270 at the NR inspection stand where the thermal neutron flux (< 0.1 eV) is $\approx 3.8 * 10^5$ n/cm².sec at 1.5 MW operating power.

L/D ratio is commonly used to describe the beam quality for a neutron radiographic beam. **L is the length from the beam aperture to the imaging plane and D is the diameter of the beam aperture that is placed inside the graphite insert.** A higher L/D ratio means the beam is more parallel and forward-directed but at a loss of flux intensity.

Neutron spectrum of the beam source end (bismuth crystal) is a typical Maxwellian distribution of neutrons at 40 °C.

Materials List:

- | | |
|-----------------------|-------------------------------|
| ¼"-thick Al-2024 | x 1 piece (up to 5 wt% of Cu) |
| ¼"-thick steel 1020 | x 1 piece |
| 40-mil-thick Boral | x 1 piece |
| 1"-thick B_4C -poly | x 1 piece |

(Additional testing materials available)

Theory:

Total “neutron” cross section (= scattering + absorption)

$$\begin{aligned} \sigma_t &= \sigma_s + \sigma_a \\ &= (\sigma_e + \sigma_i) + (\sigma_\gamma + \sigma_f + \sigma_p + \sigma_\alpha + \dots) \end{aligned}$$

σ_t (Microscopic cross section)

of a material means its unique capability of removing neutrons, especially thermal ones, from their tracks.

Thermal neutron transmission

$$\begin{aligned} I_t &= I_o * \exp(-\sigma_t * n * x) \\ &= I_o * \exp(-\Sigma_t * x) \end{aligned}$$

Σ_t (Macroscopic cross section)
= Probability per unit path length that a neutron will interact as it moves about in a medium.

Experiments:

1. **Reactor steady at 1.5 MW operating power (>2 hrs).** [An alternative method requires a separate beam detector].
2. Record the transmission count rates for **5 minutes** (I_o and I_t , cpm) on the BF_3 detector.
3. Continue and complete the following table.

| Sample Description | Sample Thickness | I_o | I_t |
|----------------------------------|------------------|-------------|-------|
| None | ----- | $I_{o,1} =$ | ----- |
| Al 2024 | 0.64 cm / 0.25” | ----- | |
| Steel 1020 (Fe) | 0.64 cm / 0.25” | ----- | |
| Boral (B₄C+Al) | 0.1 cm / 40 mil | ----- | |
| B₄C-poly | 2.54 cm / 1.0” | ----- | |
| None | ----- | $I_{o,2} =$ | ----- |

$I_o = (I_{o,1} + I_{o,2}) / 2...$ background count rate is negligible.

$I_t = I_o * \exp(-\Sigma_t * x)$

Discussions:

1. Compare measured σ_t to corrected σ_t for thermal neutrons, what cause the discrepancy? (good counting geometry? scattered neutrons reaching BF₃ detector? impurities in sample materials?)

| | N (10 ²⁴ /cm ³) | σ_s (b) | σ_a (b) | σ_t (published) | σ_t (corrected) | σ_t (measured) |
|----------------|---|-------------------|-------------------|---------------------------|---------------------------|--------------------------|
| Al | 0.06024 | 1.49 | 0.23 | 1.720 | 1.687 | --- |
| Al (Cu) | 0.06024 | --- | --- | --- | 1.895 | |
| Cu | 0.08493 | 7.90 | 3.79 | 11.69 | 11.15 | --- |
| Fe | 0.08487 | 10.9 | 2.55 | 13.45 | 13.09 | |

Data from “Introduction of Nuclear Engineering”, J.R. Lamarsh, 3rd edition.

Effective σ_a at 40 °C = $\sigma_{0.0253 \text{ eV}, a} * \pi^{0.5} / 2 * (293/ T=313)^{0.5} = \sigma_{0.0253 \text{ eV}, a} * 0.857$

σ_t (corrected) = σ_s (approximately constant at lower energies) + $\sigma_a * 0.857$

Al 2024 has up to 5 wt% of Cu.

Atom percent ratio of Al vs. Cu... 95% / 27.0 : 5% / 63.5 = 0.978 : 0.022

Therefore, 1.687 * 0.978 + 11.15 * 0.022 = 1.895

2. Calculate the **HVL** (half value layer) of shielding materials, such as **Boral** and **B₄C-poly**, for thermal neutrons. (**I_t = 0.5 I₀**)